

Corrections to  
**Fracture Mechanics**  
Lecture Notes in Applied and Computational Mechanics, 62

Last updated March 14, 2016

Over the years I have found a number of small mistakes in my book. I hope they've not caused you any trouble. In any case, here are some corrections. There are probably other mistakes I've yet to catch. If so, let me know.

Alan Zehnder  
Ithaca NY  
atz2@cornell.edu

## Section 2.4

### p. 9

Equation (2.4) should read

$$w(x_1, x_2) = w^*(x_1, x_2)$$

### p. 11

Just after equation 2.17 it should read ... Eqns (2.16) and (2.17) predict that the stress field is singular ...

### p. 12

For consistency with Eq (2.16), on this whole page  $B_2$  should be replaced by  $B_1$  .

### p. 14

On the 2nd line it should read ... is given by  $f' = u_{,1} + iv_{,1} = \dots$

## Section 5.3

### p. 68

Equation 4.16 should be

$$\theta_0 = \lambda'(l) - \frac{\eta}{\sqrt{\pi}} \int_0^l \frac{\lambda'(x)}{(l-x)^{1/2}} dx ,$$

## Section 5.3

p. 82

Here I neglected to account for the fact that  $A_n$  in Eq. (5.7) can be complex. So let  $A_n = B_n + iC_n$ . Then the complex stress is written as

$$\tau = \sum_{n=-\infty}^{+\infty} A_n z^{\lambda_n} = \sum_{n=-\infty}^{+\infty} (B_n + iC_n) r^{\lambda_n} (\cos \lambda_n \theta + i \sin \lambda_n \theta)$$

Set the traction to zero on the crack faces, i.e.  $\text{Re}(\tau(\theta = \pm\pi)) = 0$  to get the two equations:

$$\begin{aligned} \sum r^{\lambda_n} (B_n \cos \lambda_n \pi + iC_n \sin \lambda_n \pi) &= 0 \\ \sum r^{\lambda_n} (B_n \cos \lambda_n \pi - iC_n \sin \lambda_n \pi) &= 0 . \end{aligned}$$

Add and subtract the above equations to get two sets of eigenvalues and eigenfunctions:

$$\begin{aligned} \lambda_n &= -\frac{1}{2} + n \quad , \quad C_n = 0 \\ \lambda_n &= n \quad , \quad B_n = 0 \end{aligned}$$

As discussed in the book, taking only  $\lambda_n \geq -\frac{1}{2}$  we have the Laurent series for the complex stress for a sharp anti-plane shear crack as

$$\tau = \sum_{n=0}^{\infty} B_n z^{-\frac{1}{2}+n} + iC_n z^n .$$

In this case the leading coefficient is related to the stress intensity factor by

$$B_0 = \frac{K_{III}}{\sqrt{2\pi}}$$

The boundary collocation procedure, Eq. (5.8), should read

$$\text{Im} \sum_{n=0}^p (B_n z^{-\frac{1}{2}+n} + iC_n z^n) n^k = t_3^k .$$

If you work through the assignment on this topic you may find some interesting results regarding the coefficients  $B_n$  and  $C_n$ . Try it out!

## Sec. 5.6

p. 105

In Eqn (5.38) replace  $\sigma_a$  by  $\tau_a$ .

## Sec. 6.3

p. 115

Replace MTB with MBT.

$V_L$  should be  $v_l$ .

$V_{LC}$  should be  $v_{LC}$ .  $v_{LC}$  is defined as the load-line displacement at fracture.